



# RULES AND REGULATIONS FOR THE CONSTRUCTION AND CLASSIFICATION OF FLOATING OFFSHORE UNITS

**RULES CHANGE NOTICE NO. 2** 

March 2025

Rules Change Notice No.2, March 2025

#### **General Information**

This Rules Change Notice gives the new additions and amendments to the 'Rules and Regulations for the Construction and Classification of Floating Offshore Units' along with the effective dates from which these changes are applicable.

These new additions and amendments are to be read in conjunction with the requirements given in the July, 2024 edition of the Rules and 'Rules Change Notice No.1 December, 2024'.

The Part / Chapters where amendments are made and their effective dates are indicated in **TABLE 1**. The actual requirements, arranged in the order of Part / Chapter / Section / Subsection / Clause, have been given subsequently.

For ease of reference, the newly added text has been highlighted by underlining and the deleted text by striking through.

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#### RULES AND REGULATIONS FOR THE CONSTRUCTION AND CLASSIFICATION OF FLOATING OFFSHORE UNITS- July 2024

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## TABLE 1 – AMENDMENTS INCORPORATED IN THIS NOTICE

These amendments will come into force as indicated in the Table

Section / Clause	Subject/ Amendments						
Chapter 4: Hull Structure							
The amendments are applicable to FOUs contracted for construction on or after 1 July 2025.							
7/ 7.4.4.1	.4.4.1 The $f_{v}$ factor to be used in the formula for evaluation of heave acceleration for strength assessment, and fatigue assessment is clarified.						
13/ Table 21The design load sets in Table 21 are corrected for proper correspond to the acceptance criteria provided in Table 22.							

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#### **Chapter 4**

#### Hull Structure

#### Section 7

#### **FOU Motions and Accelerations**

7.4 FOU Accelerations at the center of gravity

#### 7.4.4 Heave Acceleration

7.4.4.1 The vertical acceleration due to heave is to be taken as:

 $a_{heave} = f_V a_0 g \qquad [m/s^2]$ 

<u>Where:</u>  $f_V = 1$  for scantling requirements and strength assessment  $f_V = \left(\frac{C_{b-LC}}{C_b}\right)^2 \left(1.2 - \frac{L}{100}\right)$  for fatigue strength <u>evaluation</u> <u> $C_{b-LC}$ </u> : block co-efficient for the considered loading condition Rules Change Notice No.2, March 2025

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### Section 13

## Cargo Tank Region

Table 21 : Design load sets for plating and local support members								
Structural Member		Design Load set	Load Component	Draught	Remark			
Keel, Bottom Shell, Bilge, Side Shell, Sheer Strake		1	P <sub>ex</sub>	T <sub>sc</sub>	Sea pressure only			
		2 77	P <sub>ex</sub>	$T_{sc}$	Not proceure difference			
		<u> </u>	<u>Pin-Pex</u> <u>Pin-Pex</u>	<u>0.25<i>T<sub>sc</sub></i><b>T</b><sub>bal</sub></u> <u><i>T<sub>bal</sub></i></u>	Net pressure difference between water ballast pressure and sea pressure			
	In way of cargo tanks	<u>42</u>	P <sub>ex</sub>	T <sub>sc</sub>	Green sea pressure only for other loads on deck			
		<u>3</u>	Pin	_				
		<u>4</u> 11	Pin Pin-flood	<u>0.67<sub>sc</sub></u>	Cargo pressure only			
	In way of	4 <u>2</u>	P <sub>ex</sub>	T <sub>sc</sub>	Green sea pressure only for other loads on deck			
Deck	tanks other than cargo	<u>5</u>	<u>Pin</u>	<u>0.25<i>T</i>sc</u>	Water ballast or other			
	tanks	<u>6</u>	<u><i>P</i></u> <i>in</i>	<u>T<sub>bal</sub></u>	liquid pressure only			
	tunno	11	Pin-flood	-				
		<u>9</u> 9	P <u>dk</u> Pdk	bal	Distributed or			
	Any location	<u>10</u>	<u>P<sub>dk</sub></u>	<u>T<sub>bal</sub></u>	concentrated loads only. Simultaneously occurring green sea pressure may be ignored			
		33	Pin <sub>Pin</sub>	- <del>0.67<sub>sc</sub></del>				
		44	P <sub>in</sub> P <sub>in</sub>	<u>0.67<sub>sc</sub></u>	Cargo pressure only			
	om, Inner hull,	5	<u>Pin</u>	$\frac{0.25T_{sc}}{0.25T_{sc}}$				
Нор	Hopper side		Pin	T <sub>bal</sub>	Water ballast or other			
1		<u>11</u> 5	Pin-flood Pin	<b>T</b> <sub>bal</sub>	liquid pressure only			
		<u>3</u> 3	<u>Pin</u> Pin	<u>-0.67</u> se	Pressure from one side			
		<u>4</u> 4	<u>Pin</u> Pin	<u>0.67<sub>sc</sub>-</u>	only. Full cargo tank with			
Longitudinal bulkhead, Centerline bulkhead		11	Pin-flood	-	adjacent cargo tank empty. Two cases are to be evaluated: 1. Inner empty, outer full 2. Inner full, outer empty			
Transverse Bulkhead	In way of cargo tanks	<u>3</u> 3	<u>Pin</u> Pin	<u>-0.67</u> sc	Pressure from one side			
		<u>4</u> 4	Pin Pin	<u>0.67<sub>sc</sub>-</u>	only. Full cargo tank with			
		<u>11</u>	Pin-flood		adjacent fwd or aft cargo tank empty. Need to			
	In way of tanks other	<u>5</u> 5 66	PinPin PinPin	$\frac{0.25T_{sc}T_{sc}}{T_{bal}0.25T_{sc}}$	evaluate 2 cases			
	than cargo tanks other	<u>0</u> 0	<u>Fin</u> Pin-flood		1) Fwd empty, aft full 2) Fwd full, aft empty			
	lains	5 <del>5</del>	P <sub>in</sub> P <sub>in</sub>	0.25T <sub>sc</sub> T <sub>bal</sub>	Pressure from one side			
Other tank boundaries. e.g Girders, floors and stringers		<u>6</u> 6	P <sub>in</sub> P <sub>in</sub>	Tbal 0.25Tsc	only. Full tank with			
		<u>11</u>	<u>Pin-flood</u>	-	adjacent tank empty. Need to evaluate 2 cases, see above			

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Note:

 $T_{sc}$ : Scantling draught  $T_{bal}$ : minimum ballast draught

1. Description of design load set is provided in Table 22

2. The boundaries of void and dry space not forming part of the hull envelope are to be evaluated using Design Load Set 11.

3. The above load sets are to be checked considering on-site, transit and inspection/maintenance conditions. For transit and inspection maintenance conditions, if the draught of the unit does not correspond to draughts mentioned for the load sets mentioned above, then the consideration of draughts for the checks is to be decided by IRS.

4. For structural members/configurations not covered by above specifications, the applicable Design Load sets to determine the scantling requirements of structural boundaries are to be selected so as to specify a full tank on one side with the adjacent tank or space empty. The boundary is to be evaluated for loading from both sides. Design Load Sets are to be selected based on the tank or space contents and are to maximize the pressure on the structural boundary, the draught to use is to be taken in accordance with the Design Load Set and this table. Design Load Sets covering the S and S+D design load combinations are to be selected.

Table 22 : Design Load Set specification										
Design	Design Load Design load Acceptance Parameters for dynamic load									
Load	Component	combination	criteria set	Calculations   DLCF GM Rroll-gyr						
set	Component	combination	Ciliena set							
001				Table	0101	T Croil-gyr				
				selection						
Hull Envelope (primary and local support members)										
1	Sea Pressure	S	AC1		-					
2		S+D	AC2	Full Load	0.12 <i>B</i>	0.35 <i>B</i>				
Cargo Tank Boundaries										
3	Cargo tank	S	AC1		-					
4	pressures	S+D	AC2	Full Load	0.24 <i>B</i>	0.40 <i>B</i>				
Boundar	Boundaries of water ballast and other tanks									
5	Water ballast or	S	AC1		-					
6	other tank	S+D	AC2	Ballast	0.33 <i>B</i>	0.45 <i>B</i>				
	pressures									
7	Net pressures	S	AC1		-					
8	(ballast – sea)	S+D	AC2	Ballast	0.33 <i>B</i>	0.45 <i>B</i>				
	rimary and local su			7						
9	Distributed	S	AC1		-	_				
10	pressures and	S+D	AC2	Ballast	0.33 <i>B</i>	0.45 <i>B</i>				
	concentrated									
	loads	_								
11	Flooded	A	AC2		-					
	condition									
	(Accidental)									
	elope (primary supp		1.01	T						
12	Net pressure	S	AC1		-					
13	(Cargo – Sea)	S+D	AC2	Loaded	0.24 <i>B</i>	0.40 <i>B</i>				
14	Average	S	AC1		-	0.050				
15	pressure (cargo	S+D	AC2	Loaded	0.12 <i>B</i>	0.35B				
16	& sea)	S+D	AC2	Loaded	0.24 <i>B</i>	0.40 <i>B</i>				

#### **End of Chapter**